STICHTING MATHEMATISCH CENTRUM 2e BOERHAAVESTRAAT 49 A M S T E R D A M

Technical Note TN 20

A note on a problem of heat transport

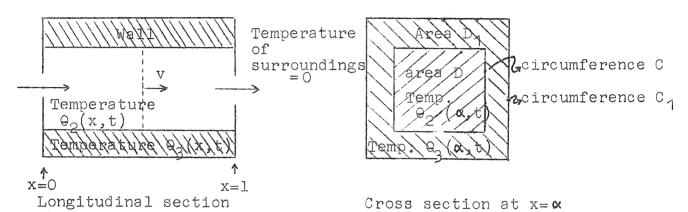
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B.R. Damsté

February 1962

A note on a problem of heat transport by B.R. Damsté.*)

The mathematical model under consideration describes the heating of a railroadcar by hot air, which is blown into it at one end (x=0) and which leaves the car at the opposite end (x=1).



For the temperature of the air entering the car, $\theta_1(t)$, we have

(1) $\theta_1(t)$ = arbitrary given function of time t. (For the particular case $\theta_1(t)$ = A(1-e^{- λ t}) see (15) seqq.) The air inside the car is thought of as moving in the x direction only, with a constant speed v. It is assumed that inside the car there is no temperature gradient normal to the x direction, so that for the temperature θ_2 inside the car we have $\theta_2 = \theta_2(x,t)$.

For x=0 we have the boundary condition

$$(2) \qquad \qquad \theta_2(0,t) = \theta_1(t)$$

The car loses heat to the wall, which again gives off heat to the environment.

The temperature inside the wall, θ_3 , is assumed to be a function of x and t, $\theta_3 = \theta_3(x,t)$, so that inside the wall

^{*)} The author wishes to thank Prof.Dr. H.A. Lauwerier for his valuable suggestions and his stimulating interest in the problem.

For a list of the symbols used see p.7.

there is no temperature gradient normal to the x direction. Furthermore we assume that inside the wall no transport of heat takes place in the x direction. The local loss of heat from the car to the wall is taken to be proportional to $\theta_2(x,t) - \theta_3(x,t)$, that from the wall to the surroundings proportional to $\theta_3(x,t)$.

The proportionality factors are \mathbf{q}_{23} and \mathbf{q}_{30} respectively per unit of area and per unit of time.

The constant temperature of the surroundings is taken as zero. For the circumferences C and $\rm C_1$ and the areas D and $\rm D_1$ see the cross section.

The specific heat of $% \left(\mathbf{q}_{2}\right) =\mathbf{q}_{2}$ air is $\mathbf{q}_{2},$ the specific heat of the wall is $\mathbf{q}_{3}.$

For t=0 we have the initial conditions

(3)
$$\theta_2(x,0) = 0$$
 and $\theta_3(x,0) = \theta_{30}(x)$.

We now introduce the constants

(4)
$$a = \frac{Cq_{23}}{Dq_2}$$
, $b = \frac{Cq_{23}}{D_1q_3}$, $c = \frac{C_1q_{30}}{D_1q_3}$.

This gives us the following simultaneous equations:

(5)
$$\begin{cases} \frac{\partial \Theta_2(x,t)}{\partial t} + v & \frac{\partial \Theta_2(x,t)}{\partial x} = -a(\Theta_2(x,t) - \Theta_3(x,t)) \\ \frac{\partial \Theta_3(x,t)}{\partial t} = b(\Theta_2(x,t) - \Theta_3(x,t)) - c\Theta_3(x,t). \end{cases}$$

By applying Laplace transformation to (5) and (6), and using the initial conditions (3), we get the system

(5a)
$$\begin{cases} p\overline{\Theta}_{2}(x,p) + v & \frac{\partial \overline{\Theta}_{2}(x,p)}{\partial x} = -a(\overline{\Theta}_{2}(x,p) - \overline{\Theta}_{3}(x,p)) \\ p\overline{\Theta}_{3}(x,p) - \Theta_{30}(x) = b(\overline{\Theta}_{2}(x,p) - \overline{\Theta}_{3}(x,p)) - c\overline{\Theta}_{3}(x,p), \end{cases}$$

in which p is the variable of Laplace transformation and the bar indicates the Laplace transform.

Elimination of θ_3 gives

(7)
$$v = \frac{\partial \overline{\Theta}_2}{\partial x} + \frac{p^2 + p(a+b+c) + ac}{p+b+c} \overline{\Theta}_2 = \frac{a - c}{p+b+c}$$

The solution of this differential equation is

(8)
$$\overline{\Theta}_2(x,p) = \overline{K}(p) \exp\left\{-\frac{p^2 + p(a+b+c) + ac}{v(p+b+c)}x\right\} + \frac{a\Theta_{30}}{p^2 + p(a+b+c) + ac}$$
 in which $\overline{K}(p)$ is a function of p which has to be determined from the boundary condition (2).

From (2) we see that

(9)
$$\overline{\Theta}_2(0,p) = \overline{\Theta}_1(p)$$
.
From (8) we get

(10)
$$\overline{\theta}_2(0,p) = \overline{K}(p) + \frac{a\theta_{30}}{p^2 + p(a+b+c) + ac}$$
.

Denoting the inverse of $\frac{a\theta_{30}}{p^2+p(a+b+c)+ac}$ by T(t) we have

$$(11) T(t) = \begin{cases} H(t) \frac{a\theta_{30}}{\sqrt{(\frac{a+b+c}{2})^2 - ac}} e^{-\frac{(a+b+c)}{t}} t \\ H(t) \frac{a\theta_{30}}{\sqrt{ac - (\frac{a+b+c}{2})^2}} e^{-\frac{a+b+c}{2}t} t \\ for (a+b+c)^2 > 4ac \end{cases}$$

$$for (a+b+c)^2 > 4ac$$

$$for (a+b+c)^2 < 4ac$$

$$H(t) a\theta_{30} t = \frac{a+b+c}{2} t$$

$$for (a+b+c)^2 = 4ac$$

In these formulae H(t) is Heaviside's unit step function $H(t) = \begin{cases} 0 & t < 0 \\ 1 & t > 0 \end{cases}$

We can easily find K(t), the inverse Laplace transform of $\overline{\mathrm{K}}(p)$, from (9), (10) and (11) as

(12)
$$K(t) = \{\Theta_1(t) - T(t)\}\ H(t)$$

For the exponential factor in (8) we have

(13) $\overline{U}(p) \stackrel{\text{def}}{=} \exp\left\{-\frac{p^2 + (a+b+c)p + ac}{v(-b+c)}x\right\} = e^{-\frac{ax}{v}} \exp\left\{\left(-\frac{p}{v} + \frac{\sqrt{v}}{p+b+c}\right)x\right\}$.

Erdélyi et al.: Tables of integral transforms I section 5.5 formula (31) gives:

$$e^{\frac{a}{r}} - 1 \neq \sqrt{\frac{a}{t}} I_1(2\sqrt{at})$$
,

so that the inverse transform of $\overline{U}(p)$ is

(14)
$$U(t) = e^{-\frac{ax}{v}} \left\{ \frac{x(t-\frac{x}{v})}{\sqrt{\frac{abx}{vt-x}}} I_1 \left(2\sqrt{\frac{abx}{v}(t-\frac{x}{v})} \right) H(t-\frac{x}{v}) \right\},$$

We thus find the following result for $\theta_2(x,t)$, in which the symbol * denotes convolution:

(15)
$$\Theta_2(x,t) = K(t) + U(t) + T(t)$$
.
For $\Theta_3(x,t)$ we have from (6) together with the boundary condition (3):

(16)
$$\theta_3(x,t) = \theta_{30} e^{-(b+c)t} + \frac{b}{b+c} \theta_2(x,t)$$
.

A particular case

We now use the heating function

(17)
$$\Theta_{\gamma}(z) = A (1-e^{-\lambda t})$$
. in which A and λ are positive constants. Then (12) becomes

(18)
$$K(t) = \{A(1-e^{-\lambda t}) - T(t)\} H(t).$$

For $\theta_2(x,t)$ we find from (15), (18) and (14)

(19)
$$\Theta_2(x,t) = T(t) + e^{-\frac{\partial x}{v}} \int_0^t \left\{ A(1-e^{-\lambda(t-\tau)}) - T(t-\tau) \right\} H(t-\tau).$$

$$\cdot \left\{ e^{-(b+c)(\tau - \frac{x}{v})} \sqrt{\frac{abx}{v\tau - x}} I_1 \left(2\sqrt{\frac{abx}{v}(\tau - \frac{x}{v})} \right) H(\tau - \frac{x}{v}) + \delta(\tau - \frac{x}{v}) \right\} d\tau.$$
For $t < \frac{x}{v}$ we have obviously

(20)
$$\Theta_2(x,t) = T(t)$$
.

Assuming now $t > \frac{x}{v}$, (19) may be reduced to

(21)
$$\theta_{2}(x,t) = T(t) + e^{-\frac{ax}{V}} \left\{ A(1-e^{--\lambda(t-\frac{x}{V})}) - T(t-\frac{x}{V}) \right\} +$$

$$+ Ae^{(-a+b+c)\frac{x}{V}} \int_{x/V}^{t} e^{--T(b+c)} \sqrt{\frac{abx}{Vt-x}} I_{1}(\frac{2}{V}\sqrt{abx(Vt-x)}) dt +$$

$$- Ae^{(-a+b+c)\frac{x}{V}} - \lambda t \int_{x/V}^{t} e^{--T(b+c-\lambda)} \sqrt{\frac{abx}{Vt-x}} I_{1}(\frac{2}{V}\sqrt{abx(Vt-x)}) dt +$$

$$- e^{(-a+b+c)\frac{x}{V}} \int_{x/V}^{t} e^{-T(b+c)} T(t-x) \sqrt{\frac{abx}{Vt-x}} I_{1}(\frac{2}{V}\sqrt{abx(Vt-x)}) dt,$$

which may be simplified to

(22)
$$\Theta_{2}(x,t) = T(t) + e^{-\frac{ax}{V}} \left\{ A(1-e^{-\lambda(t-\frac{x}{V})}) - T(t-\frac{x}{V}) \right\} +$$

$$+ Ae^{-\frac{ax}{V}} \int_{0}^{\varphi(x,t)} e^{-\frac{v(b+c)}{uabx}} w^{2} I_{1}(w)dw +$$

$$- Ae^{-\frac{ax}{V}} - \lambda(t-\frac{x}{V}) \int_{0}^{\varphi(x,t)} e^{-\frac{v(b+c-\lambda)}{4abx}} w^{2} I_{1}(w)dw +$$

$$- e^{-\frac{ax}{V}} \int_{0}^{\varphi(x,t)} e^{-\frac{v(b+c)}{4abx}} w^{2} T(t-\frac{x}{V} - \frac{vw^{2}}{4abx}) I_{1}(w)dw$$

in which $\varphi(x,t) \stackrel{\text{def}}{=} \frac{2}{v} \sqrt{abx(vt-x)}$.

The temperature $\theta_3(x,t)$ follows from (16).

For $t\to\infty$ the fourth term in the right-hand side of (22) converges even for $\lambda > b+c$ by virtue of the factor $e^{-\lambda t}$ with which the integral is multiplied. The other terms give no difficulties, which means that eventually a steady state is reached.

We are now going to determine the behaviour of the solution $\theta_{2}(x,t)$ as $t \to \infty$.

Since a steady state is reached, we may take $\frac{\partial \theta_2}{\partial t} = -\frac{\partial \theta_2}{\partial t} = 0$ in (5) and (6), which then become

(23)
$$\begin{cases} \tau \cdot \frac{\partial \theta_2}{\partial x} = -a(\theta_2 - \theta_3) \end{cases}$$

(24)
$$b\theta_2 = (b+c)\theta_3$$
.

Elimination of θ_3 gives

$$(25) \quad \nabla \frac{\partial \theta_2}{\partial x} = \frac{ac}{b+c} \theta_2$$

which, together with the boundary condition (2), leads to

(26)
$$\theta_2(x,t) \rightarrow A \exp\left\{-\frac{acx}{v(b+c)}\right\}$$
 for $t \rightarrow \infty$.

For the steady-state solution of $\theta_3(x,t)$ we find from (24) and (26)

(27)
$$\Theta_3(x,t) \rightarrow \frac{Ab}{b+c} \exp\left\{-\frac{acx}{\tau(b+c)}\right\}$$
 for $t \rightarrow \infty$.

List of symbols:

speed of the air inside the car. v: the variable of place. the variable of time. t: length of the car. 7: the variable of Laplace transformation. p: $\Theta_{\mathcal{O}}(x,t)$: the temperature of the air inside the car. $\theta_3(x,t)$: the temperature of the wall. $\theta_{30}(x)$: the initial temperature of the wall. $\theta_1(t)$: the temperature of the air which is blown into the car at x=0. constants in the equation of $\theta_1(t)$. A, λ : the loss of heat from the inside of the car to q23: the wall is proportional to q_{23} per unit of area and per unit of time. the loss of heat from the wall to the surroundings q30: is proportional to \mathbf{q}_{30} per unit of area and per unit of time. specific heat of air. q2: q₃: C: specific heat of wall. inner circumf race of cross section of car wall. 11 11 11 11 11 11 C1: area of cross section of car interior. D: " " wall. D1: $\frac{cq_{23}}{Dq_{2}}$, b: $\frac{c^{2}}{1+\frac{3}{3}}$, c: $\frac{c_{1}q_{30}}{D_{1}q_{3}}$. a:

 $\left\{ \begin{array}{l} \overline{\Theta}_2(x,p) \\ \overline{\Theta}_3(x,p) \end{array} \right\}$: the bar indicates the Laplace transform of the function.